

Application of

optimization on manifolds

to nonlinear shell theory

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Kinematics of a nonlinear Reissner-Mindlin shell model



Energy contributions



BISCHOFF (1999)

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Outline



Brief review of the kinematics of a nonlinear Reissner-Mindlin shell model

Challenges for a consistent formulation

Overcoming these challenges with optimization on manifolds

Kinematics of a nonlinear Reissner-Mindlin shell model



Kinematics



$$\begin{aligned} \mathbf{X} &= \mathbf{\Phi}_0(\xi^1, \xi^2, \xi^3) = \boldsymbol{\varphi}_0(\xi^1, \xi^2) + \xi^3 \mathbf{t}_0(\xi^1, \xi^2) \\ \mathbf{x} &= \mathbf{\Phi}_t(\xi^1, \xi^2, \xi^3) = \boldsymbol{\varphi}(\xi^1, \xi^2) + \xi^3 \mathbf{t}(\xi^1, \xi^2) \end{aligned}$$

Mappings:

$$oldsymbol{\chi}_t = oldsymbol{\Phi}_t \circ oldsymbol{\Phi}_0^{-1}, \quad oldsymbol{\chi}_t : egin{cases} \mathcal{B}_0 o \mathcal{B}_t \subset \mathbb{R}^3 \ oldsymbol{\xi} \mapsto \mathbf{x} = oldsymbol{\chi}_t(\mathbf{X}) \end{cases}$$

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Kinematics of a nonlinear Reissner-Mindlin shell model

Kinematic assumptions

Geometry approximation:

 $\mathbf{x} = \mathbf{\Phi}_t(\xi^1, \xi^2, \xi^3) = \boldsymbol{\varphi}(\xi^1, \xi^2) + \xi^3 \mathbf{t}(\xi^1, \xi^2)$

- First order transverse shear effects are taken into account:
 - The director field $t(\xi^1,\xi^2)$ is independent of the midsurface field $\varphi(\xi^1,\xi^2)$ (in contrast to Kirchhoff-Love)
- Thickness change is not contained in kinematic description:
 - The director is a unit vector, i.e. $\mathbf{t}: \mathcal{A} \to \mathcal{S}^2 \subset \mathbb{R}^3$ $\mathcal{S}^2 = \{ \mathbf{x} \in \mathbb{R}^3 \mid | \mathbf{x} \cdot \mathbf{x} = 1 \}$

Discretization

•

- Discretization of the midsurface field $\varphi: A \to \mathbb{R}^3$ trivial since it maps onto a vector space \mathbb{R}^3
- Discretization and parametrization of the director field $t: A \to S^2$ difficult due to the nonlinear space S^2





Challenges



Interpolation on the unit sphere

(Algebraic) optimization on manifolds

Update of nodal values

Interpolation: Review of historic approaches

(for non-linear Reissner-Mindlin shell formulations)

Interpolation: Review of existing approaches

Baustatik und Baudynamik

Angles

- The unit sphere can be parameterized with an angle pair $(\alpha,\beta) \rightarrow \beta$
 - The resulting interpolation is, e.g. RAMM (1976)

$$\mathbf{t} = \sum_{A=1}^{n} N^{A}(\xi) \mathbf{R}_{A}(\alpha^{A}, \beta^{A}) \mathbf{t}_{0}^{A}, \quad \mathbf{t}_{A} = \mathbf{R}_{A} \mathbf{t}_{0}^{A}$$

• Singularities, violates objectivity, unit length constraint violated

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\mathbf{t} = \mathbf{R}(\alpha,\beta)\mathbf{t}_0, \ \mathbf{R}(\alpha,\beta) \in \mathcal{SO}(3)
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RAMM (1976), ARGYRIS(1982), BAŞAR ET AL(1992), WRIGGERS & GRUTTMANN (1993)



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Interpolation: Review of existing approaches



Direct interpolation of the current nodal directors in the embedding space

- Standard interpolation formula for finite elements in vector spaces
 - Simple straightforward interpolation

HUGHES & LIU (1981), BATHE & BOLOURCHI (1980), BETSCH & STEINMANN (2002), BENSON ET AL (2010)

- $\mathbf{t} = \sum_{A=1}^{n} N^{A}(\xi) \mathbf{t}_{A}$
- Interpolated value does not lie on the unit sphere
- Objective



Interpolation: Review of existing approaches



Generalized Spherical Linear interpolation (SLERP)

• SLERP: Interpolation between two unit vectors $\mathbf{t}_1, \mathbf{t}_2$

$$\mathbf{t} = \text{SLERP}(\mathbf{t}_1, \mathbf{t}_2, \xi^1) = \frac{\sin((1 - \xi^1) \arccos(\mathbf{t}_1 \cdot \mathbf{t}_2))}{\sin(\arccos(\mathbf{t}_1 \cdot \mathbf{t}_2))} \mathbf{t}_1 + \frac{\sin(\xi^1 \arccos(\mathbf{t}_1 \cdot \mathbf{t}_2))}{\sin(\arccos(\mathbf{t}_1 \cdot \mathbf{t}_2))} \mathbf{t}_2,$$

• Generalization for four vectors in 2D

 $\mathbf{t} = \text{SLERP}[\text{SLERP}(\mathbf{t}_1, \mathbf{t}_2, \xi^1), \text{SLERP}(\mathbf{t}_3, \mathbf{t}_4, \xi^1), \xi^2]$ Areias (2013)

- Complicated interpolation
- Objective



Directors have unit length

Interpolation: Desired Properties



- Objective
- Singularity-free
- Useable for arbitrary polynomial order
- Invariant to node numbering
- Unit length in the domain



Geodesic Finite Elements SANDER (2012)

- GFE define a class of finite elements to interpolate on manifold
 - Consider the following interpolation scheme

$$\mathbf{x}^{*}(\boldsymbol{\xi}, \mathbf{x}_{i}) = \arg\min_{\mathbf{x} \in \mathbb{R}^{n}} f(\mathbf{x}, \boldsymbol{\xi}; \mathbf{x}_{i}) \qquad f(\mathbf{x}, \boldsymbol{\xi}; \mathbf{x}_{i}) = \sum_{i=1}^{n} N^{i}(\boldsymbol{\xi}) ||\mathbf{x}_{i} - \mathbf{x}||^{2}$$

$$Identical to standard interpolation!$$

$$\cdot \quad \text{Since:} \quad \frac{\partial f(\mathbf{x}, \boldsymbol{\xi}; \mathbf{x}_{i})}{\partial \mathbf{x}} \stackrel{!}{=} \mathbf{0} = \sum_{i=1}^{n} N^{i}(\boldsymbol{\xi})(\mathbf{x}_{i} - \mathbf{x}) = \sum_{i=1}^{n} N^{i}(\boldsymbol{\xi})\mathbf{x}_{i} - \sum_{i=1}^{n} N^{i} \mathbf{x} \qquad \mathbf{x}^{*} = \sum_{i=1}^{n} N^{i}(\boldsymbol{\xi})\mathbf{x}_{i}$$

- Euclidean distance can be generalized for the manifold ${\cal M}$

$$\mathbf{x}^* = \arg\min_{\mathbf{x} \in \mathcal{M}} \sum_{i=1}^n N^i(\boldsymbol{\xi}) \operatorname{dist}(\mathbf{x}_i, \mathbf{x})_{\mathcal{M}}^2 = \mathbf{x}_{GP}$$

- objective since distances are a priori rotational invariant
- Directors have unit length
- Implicit interpolation by minimization problem \rightarrow Nonlinear minimization problem at each integration point



Projection-Based Finite Elements GROHS ET AL (2019)

- Projection-based interpolation is a special kind of geodesic finite elements
 - In contrast to the GFE definition

$$\mathbf{x}^* = \arg\min_{\mathbf{x}\in\mathcal{M}}\sum_{i=1}^n N^i(\boldsymbol{\xi})\operatorname{dist}(\mathbf{x}_i,\mathbf{x})_{\mathcal{M}}^2 = \mathbf{x}_{GP}$$

• PB finite elements use the distance of the embedding space

$$\mathbf{x}^* = \arg\min_{\mathbf{x}\in\mathcal{M}}\sum_{i=1}^n N^i(\boldsymbol{\xi})\operatorname{dist}(\mathbf{x}_i, \mathbf{x})_{\mathbb{R}^n}^2 = \mathbf{x}_{GP}$$

- objective since distances are a priori rotational invariant
- Directors have unit length
- Implicit interpolation by minimization problem



 \mathbf{t}_2

What does all that mean for the unit sphere?

Example with two directors:

• **NFE**/Standard interpolation:

$$N^{1}(\xi) = 1 - \xi, \quad N^{2}(\xi) = \xi$$

 \mathbf{t}_1

$$\mathbf{I}_{\mathrm{GP}} = \sum_{i=1}^{n} N^{i}(\xi) \mathbf{t}_{i} = \arg \min_{\mathbf{t} \in \mathbb{R}^{n}} \sum_{i=1}^{n} N^{i}(\xi) ||\mathbf{t}_{i} - \mathbf{t}||^{2}$$

• Projection-Based (PBFE): GROHS ET AL (2019)
•
$$\mathbf{t}_{\text{GP}} = \arg\min_{\mathbf{t}\in\mathcal{S}^2}\sum_{i=1}^n N^i(\xi)\operatorname{dist}(\mathbf{t}_i,\mathbf{t})_{\mathbb{R}^n}^2$$

 $= \arg\min_{\mathbf{t}\in\mathcal{S}^2}\sum_{i=1}^n N^i(\xi)||\mathbf{t}_i - \mathbf{t}||^2 = \frac{\sum_{i=1}^n N^i(\xi)\mathbf{t}_i}{||\sum_{i=1}^n N^i(\xi)\mathbf{t}_i||}$

• Geodesic Finite Elements (GFE): Sander (2012) • $\mathbf{t}_{\text{GP}} = \arg\min_{\mathbf{t}\in\mathcal{S}^2}\sum_{i=1}^n N^i(\xi)\operatorname{dist}(\mathbf{t}_i,\mathbf{t})_{\mathcal{S}^2}^2$ $= \arg\min_{\mathbf{t}\in\mathcal{S}^2}\sum_{i=1}^n N^i(\xi)\operatorname{arccos}(\mathbf{t}_i\cdot\mathbf{t})^2$

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What does all that mean for the unit sphere?

Example with two directors:



Comparison of interpolation schemes

Roll-up of clamped beam

• 16 Iterations of Newton's method to reach equilibrium



Roll-up of clamped beam

• 16 Iterations of Newton's method to reach equilibrium





Roll-up of clamped beam

- Reference plane → Reference interpolation identical
- Q1 shell elements, C^{0} -continuity between elements
- Moderate initial slenderness $L/h = 12 \rightarrow$ Moderate locking





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Roll-up of clamped beam $\perp h$ MReference plane \rightarrow Reference interpolation identical Quadratic p = 2 B-spline shell elements, C^1 -continuity between elements • LModerate initial slenderness $L/h = 12 \rightarrow$ Moderate locking ٠ deformed 10^{1} M^{mod} \mathbf{PBFF} Absolute tip rotation error 10^{0} undeformed \mathbf{NFF} GFE 10^{-1} 10^{-2} $E = 1000 \, \rm kN \, cm^{-2}$ $L = 12 \,\mathrm{cm}$ 10^{-3} $b = 1 \,\mathrm{cm}$ h varying 10^{-4} clamped $\nu = 0$ 3 10^{-5} 10^{-6} Convergence order degenerates! 10^{-7} 10^{-8} 10 100 1000 Number of elements

Interpolation: Numerical experiments





M

 $\perp h$

L

Roll-up of clamped beam

- Reference plane → Reference Interpolation identical
- Quartic p = 4 B-spline shell elements, C^3 -continuity between elements
- Moderate initial slenderness $L/h = 12 \rightarrow$ Moderate locking



Challenges



Interpolation on the unit sphere

(Algebraic) optimization on manifolds

Update of nodal values

Algebraic optimization on manifolds

Algebraic optimization on manifolds

Literature



ABSIL PA, MAHONY R, SEPULCHRE R (2008) OPTIMIZATION ALGORITHMS ON MATRIX MANIFOLDS. PRINCETON UNIVERSITY PRESS, DOI:10.1515/9781400830244

BOUMAL N (2020) AN INTRODUCTION TO OPTIMIZATION ON SMOOTH MANIFOLDS. AVAILABLE ONLINE, LINK





Algebraic optimization on manifolds



(Algebraic) Problem statement



Riemannian gradient (exploiting embedding information)

Algebraic optimization on manifolds



Toy problem, gradient and Riemannian gradient



Algebraic optimization on manifolds



Riemannian Gradient: submanifolds

$$f(\mathbf{x}): \mathcal{M} \to \mathbb{R}$$
 $\overline{f}(\mathbf{x}): \mathbb{R}^n \to \mathbb{R}$

"For Riemannian submanifolds, the Riemannian gradient is the orthogonal projection of the "classical" gradient to the tangent spaces."

BOUMAL N (2020) AN INTRODUCTION TO OPTIMIZATION ON SMOOTH MANIFOLDS.

 $\operatorname{grad} f(\mathbf{x}) = P_{\mathbf{x}} \operatorname{grad} \overline{f}(\mathbf{x})$



- No charts
- No artificial singularities
- Simple linearization

Challenges



Interpolation on the unit sphere

(Algebraic) optimization on manifolds

Update of nodal values

Update of nodal values

Algebraic optimization on manifolds

Update of nodal values

 $\mathbf{x}_k + \Delta \mathbf{x}_k \not\in \mathcal{M}$

Geodesics generalize the concept of straight lines



The exponential map creates the *unique* geodesic curve starting at \mathbf{x}_k in direction $\Delta \mathbf{x}_k$ with constant speed

 $\gamma(t) = \exp_{\mathbf{x}_k}(t\Delta \mathbf{x}_k)$ $\mathbf{x}_{k+1} = \exp_{\mathbf{x}_k}(\Delta \mathbf{x}_k)$

Along these geodesics one could perform e.g. line search

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Update of nodal values

ABSIL PA, "OPTIMIZATION ON MANIFOLDS: METHODS AND APPLICATIONS", LEUVEN, 18 SEP 2009.

Luenberger (1973), Introduction to linear and nonlinear programming. Luenberger mentions the idea of performing line search along geodesics, "*which we would use if it were computationally feasible (which it definitely is not)*".



Generalize the concept of the exponential map \rightarrow Retractions

$R_{\mathbf{x}}^{\exp}(\Delta \mathbf{x}) = \exp_{\mathbf{x}}(\Delta \mathbf{x}) = \cos(||\Delta \mathbf{x}||)\mathbf{x} + \frac{\sin(||\Delta \mathbf{x}||)}{||\Delta \mathbf{x}||}\Delta \mathbf{x}$

Update of nodal values

Retractions for the unit sphere





 $R_{\mathbf{x}}^{\mathrm{rrn}}(\Delta \mathbf{x}) = \frac{\mathbf{x} + \Delta \mathbf{x}}{||\mathbf{x} + \Delta \mathbf{x}||}$



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Algebraic optimization on manifolds



Update of nodal values

Retractions for the unit sphere

Algebraic optimization on manifolds



Toy problem: Newton's method, iteration count vs. gradient norm



Simulations

Simulation of magnetic vorticies



Simulation elastic deformation of shells



Simulation of magnetic vorticies



Simulation elastic deformation of shells

Riemannian Trust-Region method



Minimizers for cylinder buckling

Simulation of Reissner-Mindlin shells



Simulation elastic deformation of shells





Simulation of Reissner-Mindlin shells



Simulation elastic deformation of shells 50 load steps

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Simulation of Reissner-Mindlin shells

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Simulation elastic deformation of shells

Several load steps



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Deformation (x1): displacement of NumPro, step 0.1.

Other physical problems



Simulation of micromagnetics

Maxwell's equation in vacuum and matter

 $\mathbf{B} = \mu_0 \mathbf{H}$ Ω $\operatorname{div} \mathbf{B} = 0$ $\nabla \times \mathbf{H} = 0$ \mathcal{B} $\mathbf{B} = \mu_0 (\mathbf{M} + \mathbf{H})$ $\operatorname{div} \mathbf{B} = 0$ $\nabla \times \mathbf{H} = 0$

Other physical problems



Simulation of micromagnetics



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Other physical problems



Simulation of micromagnetics



Application of optimization on manifolds to nonlinear shell theory



Summary

- Historical approaches can be outperformed by interpreting the problem as optimization on manifolds
- Interpolation must stay on the manifolds
- Lots of customization points exist, e.g., retractions
- Many other manifolds can be found in literature
- Methods can be used for other physical simulations (micromagnetics)

Not mentioned:

Examples:

The important Sobolev space $W^{1,2}(\Omega, \mathcal{M})$ does not even always possess the structure of a Banach manifold Geodesics for interpolation are not always unique

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Thank you!



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