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Fakultät für Bau- und Umweltingenieurwissenschaften

Motivation

In Finite Element Analysis (FEA), tetrahedral elements are very attractive to use in 3-D mesh generation due to automatized mesh algorithms. However, the FEA with these elements encounter a big challenge: Volumetric locking. The studies showed that volumetric locking can occur even in fine meshes. In contrast, higher convergence rates in terms of displacement results are observed when higher-order displacement-based elements are used. However, the spurious modes lead stress results to oscillate. Therefore, a new higher-order tetrahedral element formulation is required to eliminate these modes by utilizing robust and open-source C++ FEM library lkarus.

Uygar Kovanci Investigation and Mitigation of Volumetric Locking for Higher-Order

Tetrahedral

Elements

Modified Tetrahedral Element

Element stiffness matrix (k) is separated into constant and hourglass components $\nu \neq 0$ (correct material law)

 $\mathbf{k} = \mathbf{k}_c + \mathbf{k}_h$.

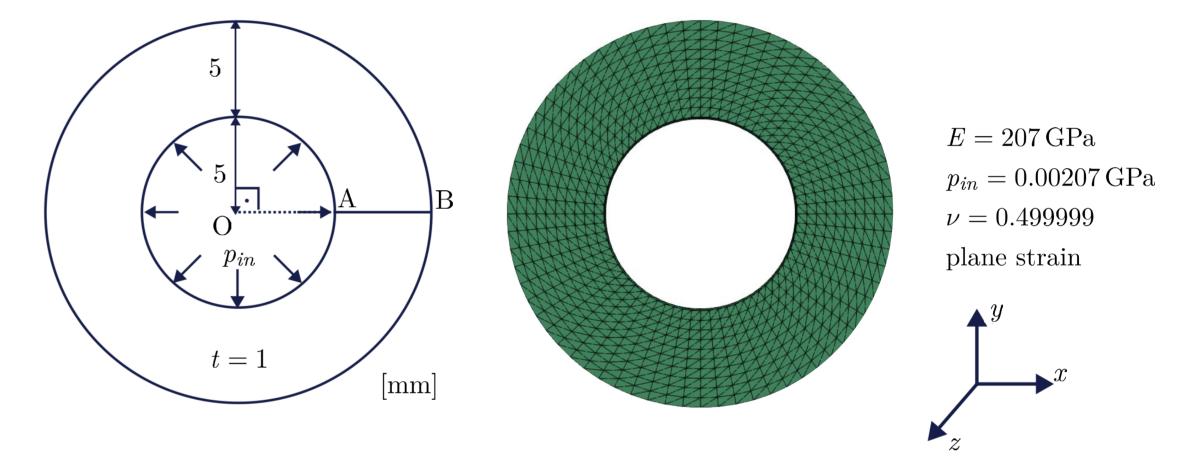
Thus, spurious modes that are dependent on Poisson's ratio are stored in the hourglass part. The same decomposition is applied to the stiffness matrix where $\nu = 0$ (false material law)

 $\mathbf{k}^0 = \mathbf{k}_c^0 + \mathbf{k}_h^0.$

If the Poisson's ratio is zero, the element has no spurious

Numerical Comparison (Thick Pipe Test)

Second-order standard tetrahedral element (TET10) and modified tetrahedral element (MTET10) are compared in terms of radial displacement, normal stresses (σ) and triaxiality (η).



mode. So, the hourglass stiffness from the correct material law is replaced by the hourglass stiffness from the false material law

$$egin{aligned} \overline{\mathbf{k}} &= \mathbf{k}_c + \mathbf{k}_h^0 \ &= \sum_{\substack{qp=1 \ \mathbf{k}^0}}^4 \mathbf{B}^{\mathrm{T}} \mathbf{C}^0 \mathbf{B} |\mathbf{J}| + \underbrace{\left(\mathbf{B}^{\mathrm{T}} (\mathbf{C} - \mathbf{C}^0) \mathbf{B} |\mathbf{J}|
ight)_{\boldsymbol{\xi}}}_{\mathbf{k}_c - \mathbf{k}_c^0}. \end{aligned}$$

Eventually, the modification affects the formulation of the stress matrix as

$$\overline{\boldsymbol{\sigma}} = \boldsymbol{\sigma}_{c} + \boldsymbol{\sigma}_{h}^{0}$$

$$= \mathbf{C}^{0} \mathbf{B} \mathbf{d} \Big|_{\boldsymbol{\xi}_{\mathrm{GP}}} + (\mathbf{C} - \mathbf{C}^{0}) \mathbf{B} \mathbf{d} \Big|_{\boldsymbol{\xi}}$$

$$\underbrace{\boldsymbol{\sigma}_{0}}_{\boldsymbol{\sigma}_{c}} - \underline{\boldsymbol{\sigma}_{c}^{0}}_{\boldsymbol{\sigma}_{c}}$$

Conclusion

Figure 1: Dimensions and mesh configuration of thick pipe model (DOFs: 6336)

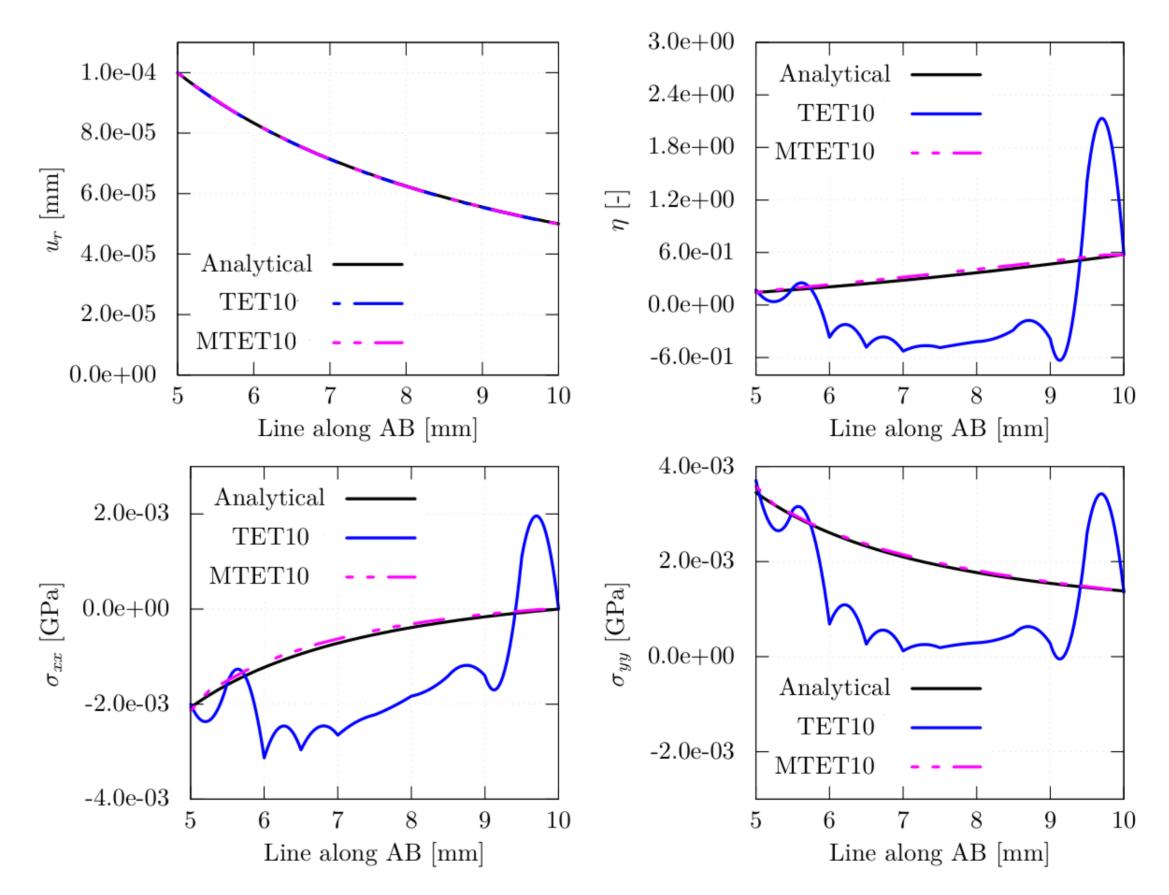


Figure 2: Radial displacement, stresses in x- and y-directions, triaxiality results along AB line

Literature

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The modified TET10 (MTET10) is locking-free and oscillatory behavior of stress results due to locking is eliminated. The results of the thick pipe test are almost aligning with the analytical results even in very coarse meshes. Thus, in engineering and scientific applications of nearly incompressible materials, one can opt for MTET10 element to obtain precise results.

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